





The Blended Wing Body (BWB) Aircraft Configuration

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Die Blended Wing Body (BWB) Flugzeugkonfiguration

Prof. Dr.-Ing. Dieter Scholz, MSME

in Zusammenarbeit mit allen Flugzeugbaukollegen des Departments Fahrzeugtechnik und Flugzeugbau



Contents



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Introduction

Projects Aero. Disciplines

Air Transport System

AC20.30

Summary

BWB Definition Strategic Targets Potential Advantages

BWB Projects Preliminary Sizing Aerodynamics Flight Mechanics Structures Mass Prediction System Integration Ground Handling Emergency Wake Turbulence Interior Design

AC20.30: Test Flights Wind Tunnel Tests Summary



Acknowledgement



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Data for this presentation was obtained from:

Internet Literature Diplomarbeiten / Master Thesis Team Effort at HAW Airbus Personal Communication







Introduction



BWB Definition



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- 1) Conventional Configuration: "Tube and Wing" or "Tail Aft" (Drachenflugzeug)
- 2) Blended Wing Body (BWB)
- 3) Hybrid Flying Wing
- 4) Flying Wing

The Blended Wing Body aircraft is a blend of the tail aft and the flying wing configurations: A wide lift producing centre body housing the payload blends into conventional outer wings.







BWB <u>target</u> advantages compared to todays advanced aircraft (from different internet sources)

reduction in weight :

better L/D :

reduction in fuel consumption :

reduction in emissions :

reduction in noise :

increase of airport capacity :

reduction in DOC :

10 to 15% less per pax 20 to 25% better **30% less** than today NOX down 17% only with engines on top more than 750 pax per A/C down 12%

DOC: Direct Operating Costs







BWB Projects





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Aerospatiale "Megajet"



Design study,1995: 1000 seats, range 6450 NM, span 96 m, cruise at Mach 0.85.







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Boeing BWB-250 ... BWB-550



Boeing: study of BWB aircraft family

Today BWBs are not a topic anymore at Boeing for civil transport!





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Boeing BWB-450



Blended Wing Body systems studies based on BWB-450 as part of the programme Ultra Efficient Engine Technology (UEET): Boundary Layer Ingestion (BLI) inlets with Active Flow Control (AFC).



NASA/CR-2003-212670





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Boeing X-48B



<u>2006</u>: Boeing, NASA, U.S. Air Force. 21 ft span wind tunnel and flight test model. Two X-48B are built. Original:

450 seats, range 7000 NM, span 75.3 m, cruise: high subsonic.











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Boeing X-48B - tanker







Air Force Research Laboratory (AFRL)





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Boeing X-48B - tanker



The X-48B prototypes have been dynamically scaled to represent a much larger aircraft. X-48B prototypes were built for Boeing Phantom Works by Cranfield Aerospace Ltd.







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TsAGI (Russia) Integrated Wing Body (IWB)



Best configuration from comparison of four New Large Aircraft configurations based on VELA specification.

Research sponsored by AIRBUS INDUSTRIE

AIRCRAFT DESIGN, Vol 4 (2001)







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5th Framework Programme of the European Commision:



1999 - 2002



17 partners: D, F, UK, E, I, NL, CZ, P

Very Efficient Large Aircraft (VELA)

Two datum configurations for a flying wing (VELA 1 and VELA 2).

Passenger-carrying aircraft.

Multidisciplinary Optimisation of a BWB (MOB) Freighter version.





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VELA 1







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VELA 2







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6th Framework Programme of the European Commision: NACRE with PDA (VELA follow on)



2003 - 2006

- WP3: Payload Driven Aircraft (VELA 3)
- WP4: Flying scale model for novel aircraft configuration





National: LuFo III, K2020

BWB (VELA 2) der Uni Stuttgart





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VELA 3









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HAW Student Project: AC 20.30





Wing profile: MH-45 (Martin Hepperle) t/c = 9.85%, low drag, improved max. lift, low $c_{m, c/4}$, proven even at Reynolds numbers below 200000. Body profile: MH-91.



AC 20.30: geometry is based on VELA 2; student project; sponsor: "Förderkreis"





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Research: Green Freighter GF - Grüner Frachter Entwurfsuntersuchungen zu umweltfreundlichen

und kosteneffektiven Frachtflugzeugen mit unkonventioneller Konfiguration





Forschung an Fachhochschulen mit Unternehmen



Bundesministerium für Bildung und Forschung







Aeronautical Disciplines







VELA 2 Technical Data

Requirements:



3-class seating: 750 pax (22 / 136 / 592) cargo capacity > 10 t

range: 7500 NM (200 NM to alternate, 30 min. holding, 5% trip fuel allowance)

high desity seating: 1040 pax

cruise Mach number: 0.85 M_{MO} : 0.89

span < 100 m





Preliminary Sizing



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Input Parameters for Preliminary Sizing

Estimation of maximum glide ratio *E* = *L/D* in normal cruise

A :	aspect ratio
S _{wet} :	wetted area
S _W :	reference area of the wing
e :	Oswald factor; passenger transports: $e \approx 0.85$

$$E_{max} = k_E \sqrt{\frac{A}{S_{wet} / S_W}}$$

$$k_E = \frac{1}{2} \sqrt{\frac{\pi e}{c_f}} = 14.9$$

$$\overline{c_f} = 0.003$$

from statistics: $k_E = 15,8$

S _{wet} / S _W :	conv. aircraft BWB	6.0 6.2 ≈ 2.4
A :	conv. aircraft	7.0 10.0
	VELA 2	5.2

E_{max} = 23,2



Preliminary Sizing



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Input Parameters for Preliminary Sizing

Estimation of maximum glide ratio *E* = *L/D* in normal cruise



TsAGI for AIRBUS



Preliminary Sizing



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Input Parameters for Preliminary Sizing

Estimation of maximum lift coefficient take-off and landing

$$C_{L,max} = C_{L,0} + \frac{\partial C_L}{\partial \alpha} \alpha + \frac{\partial C_L}{\partial \eta_W} \eta_W + \frac{\partial C_L}{\partial \eta_B} \eta_B = 0.73$$

Wind tunnel measurements of AC 20.30:









VELA 2

Assumptions:

OEW / MTOW = 0,5 LOFTIN: 0,52 (T/W!) A380: 0,49 VELA 2: $0.55 \rightarrow 0$
--

SFC = 1.4 mg/(Ns) latest technology assumed (GEnx)

approach speed = 165 kt

mass of pax and luggage for long distance flying: 97.5 kg per pax

Given:

Wing Area:

1923 m²







VELA 2









VELA 2

Sizing Results:

L/D during 2. segme L/D during missed a $V/V_{rad} = 1.09$	ent: 17.0 approach: 1	(higher than conv. due to small lift coefficient and small drag). 1.0 (normal, because landing gear drag dominates, FAR!) (normal: $V/V_{rad} = 1.0$ 1.316) => $F = 22.8$
lift coefficient cruise	: 0.25	
trust to weight ratio:	0.28	(value is slightly high for 4-engined A/C, reason: TOFL and C_1)
wing loading: 260 kg	g/m²	(very low for passenger transport, due to low lift coefficient)
Initial Cruise Altitude	e (ICA): 384	400 ft (= 11.7 km)
payload:	83000 kg]
MTOW:	501000 kg	g (VELA 2: 691200 kg)
Wing Area:	1923 m ²	² (VELA 2: 1923 m ² - forced to fit)
MLW:	366000 kg	
OEW:	251000 kg	g (VELA 2: 380600 kg)
Fuel:	167000 kg	(VELA 2: 278200 kg ?)
Thrust:	344 kN	N (for each of the four engines)





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AC20.30: CFD with FLUENT

Diplomarbeit: H. Brunswig







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AC20.30: CFD with FLUENT



path lines

Stalls can easily be handled Usable lift up to AOA of 12° At 22° AOA:

> wings are stalled body continues to produce lift but control surfaces do not deliver control power







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AC20.30: CFD with FLUENT







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AC20.30: CFD with FLUENT





Flight Mechanics



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Positioning of the CG on the Mean Aerodynamic Chord (MAC) for required static margin is achieved in conventional design by shifting the wing with respect to the fuselage. This approach is not possible in BWB design!

$$x_{LEMAC} = x_{fg} - x_{cg} + \frac{m_{wg}}{m_{fg}} \left(x_{wg} - x_{cg} \right)$$



Flight Mechanics



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Static Longitudinal Stability for VELA Configurations







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Weight Saving Potential of BWB Configurations



Helios - example of an extreme span loader with distributed propulsion (NASA / AeroVironment, Inc.)





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VELA 2 - Basic Structural Layout Thesis: T. Kumar Turai

Inner Shell made out of four quasi-cylindrical segments Intermediate double shell contour at the Leading Edge min. frame height: **Regular double shell** 200 mm contour cut by frame parallel to Leading Edge Frame height: 898;4 mm R=6000 mm Frame height: min. frame height: 200 mm 600 mm





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VELA 2 - Cabin









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VELA 2 - Wing Integration







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VELA 2 - Doors



Door cut-outs

Side door integration







VELA 2

Weight Chapter	F. Bansa	T. Kumar Turai	T. Kumar Turai (FEM)
10 Structure 20 Power Units 30/40 Systems 50 Furnishings 60 Operator Items	234669 kg 37731 kg 19795 kg 35313 kg 35313 kg	253529 kg 36603 kg 23302 kg 27588 kg 39578 kg	210070 kg -> -> ->
OWE	362820 kg	380600 kg	337141 kg
OWE/MTOW	0.525	0.551	0.488
Marckwardt	0.521		
A380-800	0.501		
A340-600	0.475		
Taken for Pre	liminary Sizing:	0.500	
Result: The BWB design does not significantly improve the OWE/MTOW ratio!			
Latest News: One-	-shell layout can	lead to OWE/MTWO	= 0.44 0.46 !



System Integration



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VELA 2 - System Installation Areas

Steps in system integration:

- 1.) System diagram
- 2.) Sizing
- 3.) Routing & ducting



System Integration



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VELA 2 - ATA 21 -Positioning of the Mixing Unit

Steps in system integration:

- 1.) System diagram
- 2.) Sizing
- 3.) Routing & ducting

Air Generation Unit is positioned in the transition wing.

Alternative position (above cabin) of the Mixing Unit eliminates riser ducts.

Ducts for recirculation air.







VELA 2 - ATA 21 - Ducting





Air circulation. Recirculation requires ducts.

Low pressure air connector and duct to mixing unit.

Duct for emergency air.



System Integration



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VELA 3 - Landing Gear Integration



Twin tandem (Bogie) nose landing gear. Two retraction mechanisms.

Two twin tri-tandem (6-wheel) main landing gears on each side.

Special retraction mechanism.

MLG wheel spacing only 11.4 m due to rib location (requirement: wheel spacing < 16 m)

Rule of Thumb: 30 t / MLG wheel => max. MTOW: 720 t







Air Transport System







VELA 3



A cargo loading vehicle drives in between the MLGs. Cargo loading from below with lifting system. Catering from the right.

Water / waste servicing on trailing edge left side.



Ground Handling



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VELA 2



Cargo loading from the right.

Catering from the right.

Boarding through three bridges.

Fuel truck under right wing.

Towing truck.



Emergency



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VELA 1 - Emergency Evacuation - Slides - Ditching



This modification of VELA 1 allows also evacuation after ditching (into the water) through over wing doors.

VELA 1, 2, 3 standard configuration can not be certified, because doors will be submerged.

Slides on forward doors.



Wake Turbulence



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Wake Turbulence - Fundamentals

Wing tip vortices cause induced drag, *D*_i.

Wake turbulence cause a danger to following aircraft.

The initial strength of the wake turbulence is based on basic aircraft parameters:



Decay of wake turbulence from a conventional wing and a C-wing.

$$P_{wake} = D_i V = \frac{2g^2}{\pi Ae} \frac{m(m/S)}{\rho V}$$

C-Wing-BWB:





Wake Turbulence



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Wake Turbulence - Comparison

$$\frac{P_{wake,BWB}}{P_{wake,A380}} \approx \frac{A_{A380}}{A_{BWB}} \cdot \frac{m_{MTO,BWB}}{m_{MTO,A380}} \cdot \frac{(m/S)_{BWB}}{(m/S)_{A380}} = \frac{7.53}{4.83} \cdot \frac{700}{560} \cdot \frac{341}{663} = 1.00$$

with BWB-Data from VELA 3. Result: no major problems expected.

Wake Turbulence - Separation

IFR Minimum Separation Rules on Approach (nm)

		Trailing aircraft type ^a	
Leading aircraft type ^a	Small	Large	Heavy
Small	3.0	3.0	3.0
Large	4.0	3.0	3.0
Heavy	6.0	5.0	4.0

Source: FAA [1978]

^a Small: aircraft weighting no more than 12,500 lb. (5,625 kg)

Large: aircraft weighting more than 12,500 lb. (5,625 kg) and less than 300,000 lb. (135,000 kg) Heavy: aircraft weighting in excess of 300,000 lb. (135,000 kg)

A380 interim value: 10 NM





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VELA 1 - Cabin Layout

Diplomarbeit: S. Lee



Vertical acceleration for pax on outer seats.









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Double Deck BWB







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Underfloor Usage - Artificial Windows







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BWB Center Wing Shapes from Inside









AC20.30





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Test Flights

AC20.30 Parameters

1:30
3.24 m
2.12 m
12.5 kg
2 electric driven fans
2 x 30 N
2 x 1400 W











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Test Flights

Recorded Parameters

barometric height, two temperatures voltage, current air speed, engine RPM GPS-Coordinates (=> position and ground speed) angle of attack, side slip angle 3 accelerations, 3 rotational speeds position of 4 control surfaces turn coordinator, ping, aerborne camera picture













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Wind Tunnel Tests











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CFD surface stream lines (left) Fluorescend paint in wind tunnel (right).

Lift coefficient dependend on flap angle (wing) and angle of attack.







Summary



Summary



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BWB advantages compared to todays advanced aircraft (checked now again, at the end of presentation):

reduction in weight :

better L/D :

reduction in fuel consumption : reduction in emissions : reduction in noise :

increase of airport capacity :

reduction in DOC :

But:

open certification problems : open design problems : single shell required. In this case: 8% better 10 to 15% better (not apparent from AC20.30) yes, due to L/D yes only with engines on top yes, more than 750 pax per A/C (probably no problems with wake turbulence) down ??% (mostly due to scale effect)

unstable configuration (?), ditching rotation on take-off, landing gear integration, ...

