



Hochschule für Angewandte Wissenschaften Hamburg

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AIRCRAFT DESIGN AND SYSTEMS GROUP (AERO)

Mass Estimation of Folding Wings

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Douglas Skyraider (Public Domain)



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https://youtu.be/W99w0h4oeyY



Abstract

Purpose – Review of mass increase of folding wings applied to passenger aircraft.

Methodology – Data is obtained from literature (Yarygina and Popov). Data is reworked to build new, simple equations.

Findings – Wing folds on passenger aircraft are intended to reduce wingspan at the gate. This keeps new, more efficient large-span aircraft in the original wingspan category according to the ICAO Aerodrome Reference Code. A wing fold cuts off part of the wing. The structural loads in the cut are larger if the cut is further inboard. A wing fold at the tip (is basically no fold and) adds no mass. The additional mass of a wing fold increases in good approximation linearly from tip to root. A wing fold at half-span position increases wing mass by about 33%. A one-sided fold is possible. A one-sided fold e.g. 20% from the tip has the same wing mass increase as a fold on both sides 10% from the tip (resulting in the same remaining span after folding). Stowage of an unsymmetrical aircraft with a one-sided fold is more complicated but one such fold may be mechanically simpler than two.

Research Limitations – Calculating a fold more inboard than 32% of half span is extrapolating given data.

Practical Implications – Approximating wing mass increase due to a fold can be estimated easily. The equations can be used in a spreadsheet for aircraft design optimization.







Acknowledgment (1/3)

This presentation is based on the work of the PhD student (at that time) **Maria Viktorovna Yarygina** and her supervisor **Prof. Dr. Yuri Ivanovich Popov**, both are from Moscow Aviation Institute (MAI). Their research is from 2011 and 2012. Their publications are listed on the next page.

Prof. Dr. Vladimir Zhuravlev, Moscow Aviation Institute (MAI) is coauthor of this presentation. Through all the years he helped greatly as a dear friend to find Russian publications and to translate essential parts of them.

Víctor Julián Sánchez Barreda prepared a Master Thesis: "Conceptual Design Optimization of a Strut Braced Wing Aircraft" at Hamburg University of Applied Sciences, Aircraft Design and Systems Group (AERO). Chapter 3.4.3 "Folding Wing Technology" takes up the work of Ms Yarygina and sets the equations up for use in an Excel table. Download from:

http://library.ProfScholz.de

https://nbn-resolving.org/urn:nbn:de:gbv:18302-aero2013-07-12.019

His work is referenced here as: Sanchez 2013





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Acknowledgment (2/3)

Publications of Maria Viktorovna Yarygina and Prof. Dr. Yuri Ivanovich Popov

Yarygina M.V., 2011. The Effect of Wing Folding on Airplane Performance (Влияние складывания крыла на характеристики самолёта). Abstract of a presentation at the 10th International Conference "Aviation and Space – 2011", Moscow, MAI. 8-10 November 2011, pp. 44-45.

Available from: <u>https://mai.ru/upload/iblock/cb8/cb875c083d5050ac0d975fc2eb365107.pdf</u>

Archived at: <u>https://perma.cc/33RZ-MXQ9</u>

Ророv Yu.I., Yarygina M.V., 2011. Methods for Weight Analysis of a Folding Wing of a Deck-Based Airplane. (Методика весового анализа складного крыла самолета палубного базирования.) In: Online journal "Proceedings of MAI" (Электронный журнал «Труды МАИ»), vol. 2011, no. 43 (Выпуск № 43), 23 pages.

Available from: <u>https://mai.ru/publications/index.php?ID=24860</u>

Archived at: <u>https://perma.cc/HH5T-Q7M2</u>

Yarygina M.V., Popov Yu.I., 2012a. Development of the Weight Formula for a Folding Wing (Формирование весовой формулы складного крыла). In: Aviation Engineering News of Universities (Авиационная техника. Известия высших учебных заведений), vol. 2012. no 2, pp. 8-12.

Available from: <u>https://old.kai.ru/aviatech/archive/2.12.cr.htm</u>

Archived at: <u>https://perma.cc/S8S8-TTQQ</u>







Acknowledgment (3/3)

Publications of Maria Viktorovna Yarygina and Prof. Dr. Yuri Ivanovich Popov

English version of Yarygina 2012a:

Yarygina, M.V., Popov, Y.I., 2012b. Development of the Weight Formula for a Folding Wing. In: Russian Aeronautics (Iz VUZ), vol. 55, pp. 120–126.

Available from: <u>https://doi.org/10.3103/S106879981202002X</u>

Archived at: <u>https://perma.cc/NVW3-YTB3</u>

Yarygina M.V., 2012c. Design and Weight Analysis of Structures of Folding Wing (Проектирование и весовой анализ конструкций складного крыла.) In: Online journal "Proceedings of MAI" (Электронный журнал «Труды MAИ»), vol. 2012. no. 51 (Выпуск № 51), 24 pages.

Available from: <u>https://mai.ru/publications/index.php?ID=29226</u>

Archived at: <u>https://perma.cc/SDA6-MGSR</u>

Yarygina, Maria Viktorovna. The Method of the Folding Wing's Design and Mass Optimization for the Naval Aircraft. In: 4th European Conference for Aerospace Sciences (Saint Petersburg, Russia, July 4 to 8, 2011). Belgian: EUCASS. 9 pages.

Available from: <u>https://www.eucass.eu/component/docindexer/?task=download&id=4337</u>

Archived at: <u>https://perma.cc/ZN4A-MAYB</u>







Motivation

- Wing optimization results in large wingspan. However, span is limited at airports.
- Possible solutions are:
 - => Winglets
 - => Box Wing Aircraft
 - => large-span wings in flight and **folding wings** at the gate!
- Winglets, the Box Wing Aircraft, any nonplanar wing systems have aerodynamic and structural disadvantages.
- The folding wing allows aerodynamically uncompromised, planar large wingspan.
- A wing fold adds mass. How much additional mass?
- Only **aircraft design** can give the **final answer**, if a wing fold has advantages. See presentation "Wing Design Regarding Mass and Drag" for a simple approach.





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Wingspan Limits at Airports





Wingspan Limits at Airports

ICAO Aerodrome Reference Code

Code letter	Wingspan	Typical aeroplane
А	< 15 m	PIPER PA-31/CESSNA 404 Titan
В	15 m but < 24 m	BOMBARDIER Regional Jet CRJ-200/DE HAVILLAND CANADA DHC-6
С	24 m but < 36 m	BOEING 737-700/AIRBUS A-320/EMBRAER ERJ 190-100
D	36 m but < 52 m	B767 Series/AIRBUS A-310
E	52 m but < 65 m	B777 Series/B787 Series/A330 Family
F	65 m but < 80 m	BOEING 747-8/AIRBUS A-380-800

https://skybrary.aero/articles/icao-aerodrome-reference-code

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Wingspan Limits at Airports

Airplane Design Group (ADG) by FAA

Group	Wingspan in feet (m)	Tail Height in feet (m)	Typical Aircraft
I	< 49' (15m)	< 20' (6.1m)	CESSNA 421 Golden Eagle/PIPER PA-31
II	49' (15m) - < 79' (24m)	20' (6.1m) - < 30' (9.1m)	CRJ/SAAB 340
Ш	79' (24m) - < 118' (36m)	30' (9.1m) - < 45' (13.7m)	BOEING 737-700/AIRBUS A-320/EMBRAER ERJ 190-100
IV	118' (36m) - < 171' <mark>(</mark> 52m)	45' (13.7m) - < 60' (18.3m)	B767 Series/AIRBUS A-310
V	171' (52m) - < 214' (65m)	60' (18.3m) - < 66' (20.1m)	B777 Series/B787/A330 Family
VI	214' (65m) - < 262' (80m)	66' (20.1m) - < 80' (24.4m)	BOEING 747-8/AIRBUS A-380-800

These groups are defined in FAA Advisory Circular 150/5300-13. It is sometimes used in place of the ICAO Aerodrome Reference Code. Boundaries for wingspan are identical.

https://skybrary.aero/articles/airplane-design-group-adg





Types of Wing Folds









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Types of Wing Folds

Boeing B777X

Code E: < 65 m.

B777X wingspan: 235 ft = 71.6 m

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Wing tip:
11 ft = 3.3 m
Two times:
22 ft = 6.6 m
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B777X at gate: 213 ft = 65 m

Better aerodynamics with a folding wingtip



https://www.boeing.com/commercial/777x/by-design

A wing extension is by roughly a factor 3 better than a winglet!

See: D. Scholz, https://doi.org/10.13111/2066-8201.2018.10.1.12





Types of Wing Folds

Boeing B777X – Actuation



Actuation mechanism by Liebherr Aerospace

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Types of Wing Folds

Boeing B777X – Cockpit

Folding wing tip

on the B777X Overhead Panel and on the EICAS (Engine Indicating and Crew Alerting System)



Flight Global 2017 (<u>https://perma.cc/5GEE-K59Z</u>)





Calculating Additional Mass for a Wing Fold







Assumptions

- Yarygina and Popov looked at carrier-based airplanes with folding wings. They got hold of mass statistics (no details published with their) and produced statistical equations to resemble these mass findings.
- Statistics of carrier-based airplanes may not lead to optimum results for passenger aircraft. However, there is no such data on passenger aircraft (with the exception of the B777X, but not in reach for me), so the data of carrier-based airplanes must be sufficient also for passenger aircraft.
- The most widespread folding type is the axis parallel to the Airplane Symmetry Plane (ASP). A turn is performed around the axis located on the upper wing surface along its chord. The given folding type is the most manufactured. It is safe in terms of structural design and results in the smallest mass increase.
- The axis of the fold is usually in the rib plane of a swept wing.
- The statistic is for **the simple butt joint** (one piece of wing positioned against the other).
- Often, it is necessary to change not only the wing structure, but also the wing high-lift devices (or other parts of the wing). The equations here are limited to the **direct wing fold mass increase**.





Elements of Wing Folds (1/2)



The wing bending moment is taken up by panels. The fold is designed with eye-lugs. They merge within each other like two combs. The upper eye-lugs are the folding axis, the lower eye-lugs are the pinning axis. a) MIG-29K, b) Su-33, c) actuator in the folding mechanism. (**Yarygina 2012b**)





Elements of Wing Folds (2/2)



The folding wing of the **Su-33**. The upper eye-lugs are the folding axis, the lower eye-lugs are the pinning axis. An actuation arm is visible. Hydraulics and electrics are routed through the fold to supply the outer part of the wing. Left: **Popov 2011**. Right: **Yarygina 2012c**.





Mass Contributions of Wing Folds

The wing with a fold at position *z_{fold}* consists of a Fixed Wing Section (FWS) and a Pivoting Wing Section (PWS). ASP is the Airplane Symmetry Plane. At the fold a structural section Δ*z* is structurally reinforced. This is the load-carrying insert structure between FWS and PWS, with additional mass, *m_{ins}*.



- Furthermore, there is additional mass of the folding mechanism, m_{mech,fold} and
- additional mass of the pinning mechanism, m_{mech,pin}.
- The additional mass of the actuation system (below) is included in the additional mass of the pinning mechanism.



Yarygina 2012b and 2012c





Critique (1/2)

• Yarygina builds equations from statistics from three know points of relative span position **z** or **y**/(**b**/2) at 0.32, 0.48, and 0.64. Results are polynomials of this form

$$\overline{m}_{fold}^{ins} = 0.24 \left(\overline{m}_{PWS} - 0.924 \right)^2 - 0.007 \tag{1}$$

• The equations have one independent parameter. It is not the relative span position *y/(b/2)*, but the relative size of the cross section of the torsion box at the wing fold position

$$\overline{m}_{\rm PWS}\left(z\right) = \frac{\left(b_z + b_{t.b}\right) \left(0.5l - z\right) \left(\overline{c}_z b_z + \overline{c}_{t.b} b_{t.b}\right)}{\left(b_0 + b_{t.b}\right) l_w \left(\overline{c}_0 b_0 + \overline{c}_{t.b} b_{t.b}\right)}.$$
 Yarygina 2012b

- Using the size of the torsion box may be a good idea, but statistical data is given and evaluated towards (1) based on relative span, *z* and not *m*_{PWS}(*z*).
- **y** is the absolute distance to the side (in span direction), **b** is wingspan, **b/2** is half-span.

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Critique (2/2)

Yarygina builds mass equations from statistics from three known points of relative span position, z or y/(b/2) at 0.32, 0.48, and 0.64. Results are polynomials of this form

$$\begin{array}{c} nr_{fold} = 0.21 (nr_{PWS} = 0.521) = 0.00 \\ \hline \\ 0.30 \\ 0.20 \\ 0.10 \\ 0.00 \\ 0.1 \\ 0.2 \\ 0.30 \end{array}$$

$$\overline{m}_{fold}^{ins} = 0.24 \left(\overline{m}_{PWS} - 0.924 \right)^2 - 0.007 \tag{1}$$

- Mass increase at three points is given. The equation obtained from this polynomial fit is only valid in between the three point (in the range of relative span from 0.32 and 0.64).
- Especially fold positions near the tip are relevant for passenger aircraft but cannot be calculated with (1).
- Note: Given plot is for the whole wing (left and right). (1) may calculate only the mass increase of one wing side.

Evaluation of mass data: https://doi.org/10.7910/DVN/T56NM9

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New Equation for m_{ins} Based on Given Data

Data points (Yarygina 2012b) and new equation for **relative additional mass of the load-carrying insert structure**.



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New Equation for $m_{mech,fold}$ and $m_{mech,pin}$ Based on Given Data

Data points (Yarygina 2012b) and new equation for **relative additional mass of folding mechanism** and **pinning mechanism** in a way to achieve zero additional mass at wing tip.



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Summing Up: New Equation for *m*_{fold}

A new and simple equation considering all or most effects of **relative additional mass of folding wings** as a **function of the relative span position of the wing fold**.



$$m_{fold}$$
 =
m_{ins} + m_{mech,fold} + m_{mech,pin} =
-0.659 y/(b/2) + 0.659

Note: Equations are based on data of fighters. Passenger aircraft experience smaller load factors. Accordingly, the mass increase of a wing fold of a passenger aircraft may be lower than given here.

Final equation				
	factor	ratio		
	0 274	57%		
III ins	0.374	57%0		
M mech,fold	0.220	33%		
m _{mech,pin}	0.065	10%		
	0.659	100%		

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One-Sided Wing Fold







One-Sided Wing Fold

Considering a One-Sided Wing Fold

A one-sided fold is possible. A one-sided fold e.g. 20% from the tip has the same wing mass increase as a fold on both sides 10% from the tip (resulting in the same remaining span after folding). Stowage of an unsymmetrical aircraft with a one-sided fold is more complicated but one such fold may be mechanically simpler than two folds.







Airport Considerations







Airport Considerations

Implications of Larger Wingspan (Code Letter) at Airports

Considering folding wings at airports? Or just going for a larger Code Letter (moving e.g. from C to D)?

Implications for gates:

- Gates are built according to the wingspan (code letter) of the aircraft. This determines the distance between gates along the terminal building. If (old) code C aircraft are designed with larger wingspan to yield code D aircraft, they would need to use other gates available only in smaller numbers.
 Eventually the airport terminal buildings would need to be reconstructed to serve demand for larger code letters.
- Landing fees are determined from maximum take-off mass (MTOM). Aircraft with larger span and more demand for space are initially not charged more but benefit from lower fuel burn in cruise.
 Landing fees may be calculated from MTOM and wingspan in the future, if airports get major problems due to space demands from large wingspan.

Implications for taxiways:

• Taxiways exist that are large enough for two code C aircraft to pass each other in a two-way operation. The same taxiway may allow only one-way operation for code D aircraft or larger. Larger span aircraft can lead to handling restriction at the airport.





Airport Considerations

Different Gates at Airports for Different Code Letters



Airports offer gates for aircraft with different size (wingspan and code letter) **according to demand**. Airport Charles de Gaulle, Terminal 2, Paris (Google Maps, <u>https://maps.app.goo.gl/m7iAjuBuob71wi6j9</u>)

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Airport Considerations

Folding Wing at Airport



Impression of aircraft with folding wing at airport (Scholz)

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Evaluation of mass data from Yarygina 2012b: <u>https://doi.org/10.7910/DVN/T56NM9</u> (Excel file)



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